

Chapter 2 Discussion Questions

Section 2.1

- 2.1 A *system* is a region in space having at least a volume.
- 2.2 A system needs a boundary to define the volume of that system.

Section 2.2

- 2.3 A *mole* or *mol* is a given number of molecules or atoms. Avogadro's Number is the number of molecules or atoms in one mole based on a gram. That is, one gram-mole of a substance has 6.022×10^{23} atoms or molecules, which is Avogadro's number.
- 2.4 Yes, a gram-mole is only 1/454 of a lbm-mol.

Section 2.3

- 2.5 A property helps describe a system.
- 2.6 Intensive properties of a system are properties based on one unit of mass of the system. Extensive properties describe the total system.
- 2.7 Specific energy is the energy per unit mass of a system.

Section 2.4

- 2.8 A state of a system is the complete description of a system, or the list of properties describing the system.

Section 2.5

- 2.9 A process is a change in a system's state.

Section 2.6

- 2.10 A cycle is a set of processes of a system which returns the system to its

1.3/ OPEN EES EQUATION WINDOW
AND ENTER:

{Problem 1-31}

$$W_k = p^*v^{**}1.4$$

$$p^*v = 4.56*T$$

$$W_k = Q - 0.234*T$$

$$Q = 456/T$$

$$T = 23*p$$

THEN CLICK CALCULATE AND
SOLVE TO OBTAIN:

Unit Settings: [kJ]/[C]/[kPa]/[kg]/[degrees]

$$p = 0.1708 \quad Q = 116.1 \quad T = 3.928 \quad v = 104.9$$

$$W_k = 115.2$$

No unit consistency or conversion problems were detected.

original state.

Section 2.7

- 2.11 Weight is the gravitational attraction between two bodies. The mass is a quantity of matter and weight is mass multiplied by the gravitational acceleration.
- 2.12 The term g_c is a constant of proportionality between momentum change (or mass times acceleration) and force (or weight)

Section 2.8

- 2.13 Specific volume is the volume per unit mass of a system.
- 2.14 Specific weight is the weight per unit volume of a system.
- 2.15 Specific Gravity is the ratio of the density of a substance to that of water at 4°C , standard atmospheric pressure of 1 bar.
- 2.16 Density is the mass per unit volume, or inverse specific volume.
- 2.17 Gage pressure is the pressure measured by a gage, usually when the gage is placed in a standard atmosphere of 1 bar pressure. It is a difference in pressure between absolute pressure of a system and the atmospheric pressure. Gage pressure is the pressure "felt" by a system at its boundary.

Section 2.9

- 2.18 The zeroth law of thermodynamics makes a temperature measurement independent of a system. Thus, a temperature of, say 30 degrees, is the same anywhere and anytime.

Section 2.10

- 2.19 Temperature is a measure of the "hotness" of a system.
- 2.20 A thermopile a group of thermocouples, all connected in series to each other.

Section 2.11

- 2.21 Energy is the capacity of a system to affect changes to its surroundings.
- 2.22 Internal energy is the form of energy manifested by the hotness or temperature, or the thermal energy. It is the kinetic energy of the individual atoms or molecules making up the system.

Section 2.12

- 2.23 Some outputs from a system would be, for instance, power produced by an engine, amount of water boiled in a boiler, or an amount of air pressurized in an air compressor.
- 2.24 Some inputs to a system would be, for instance, rate of fuel used by an engine, amount of energy used by a boiler, or power to drive a compressor.

Section 2.13

- 2.25 A derived unit is a unit or combination of fundamental units for describing a particular property or quantity.

CHAPTER 2

THE PROBLEMS IN SECTIONS 2.7 AND 2.8 ARE INTENDED TO HELP UNDERSTAND THE CONCEPTS OF WEIGHT, MASS, VOLUME, DENSITY, SPECIFIC VOLUME, AND PRESSURE.

2.1 WEIGHT $W = mg$. THUS, AT $g = 9.8 \text{ m/s}^2$

$$W = (2 \text{ kg})(9.8 \text{ m/s}^2) = 19.6 \text{ Newtons}$$

(N)

AT $g = 9.78 \text{ m/s}^2$

$$W = (2 \text{ kg})(9.78 \text{ m/s}^2) = 19.56 \text{ N}$$

SO THAT THE GOLD CUBE HAS GREATER WEIGHT AT LOCATION WHERE $g = 9.8 \text{ m/s}^2$.
THE MASS IS THE SAME AT BOTH LOCATIONS.

2.2 $W = mg = (3 \text{ kg})(9.79 \text{ m/s}^2) = \underline{\underline{29.37 \text{ N}}}$

2.3 $W = mg/g_c$ FOR ENGLISH ENGR. UNITS.

SO THAT $m = Wg_c/g$.

AT SEA LEVEL $g = 32.174 \text{ ft/s}^2$ SO THAT

$$m = (8.333 \text{ lb}_f) \left(\frac{32.174 \text{ ft} \cdot \text{lb}_f}{16 \text{ ft} \cdot \text{s}^2} \right) / (32.174 \text{ ft/s}^2)$$

$$\underline{m = 8.333 \text{ lb}_m}$$

ALSO, $32.174 \text{ lb}_m = 1 \text{ slug}$ SO THAT

$$\underline{m = 8.333/32.174 = 0.2589... \text{ SLUGS}}$$

2.4 THE MASS OF THE BATTERY IS THE SAME ON THE EARTH AND ON THE MOON.

$$m = W g_e / g = \frac{(32 \text{ lb}_f)(32.174 \text{ ft-lb}_m/\text{lb}_m \cdot \text{s}^2)}{(32.174 \text{ ft/s}^2)}$$
$$= 32 \text{ lb}_m.$$

ON THE MOON, WHERE $g = 5.47 \text{ ft/s}^2$

$$W = mg_e / g = (32 \text{ lb}_m)(5.47) / (32.174)$$

$$\underline{W = 5.44... \text{ lb}_f}$$

2.5 (a.) $1 \text{ lb}_m = 453.59 \text{ grams} \approx 454 \text{ grams}$

(b.) $2 \text{ lb}_m = 2 \times 0.45359 \text{ kg} = 0.90718 \text{ kg}$

(c.) POUNDS-FORCE IS A FORCE OR WEIGHT UNIT. IF $g = 32.174 \text{ ft/s}^2$ AND SINCE 20 SLUGS IS A MASS, WE HAVE

$$W = mg = (20 \text{ SLUGS})(32.174 \text{ ft/s}^2)$$
$$\underline{= 643.48 \text{ lb}_f}$$

(d.) DYNE IS A FORCE OR WEIGHT UNIT.

IF $g = 9.8 \text{ m/s}^2$ AND $m = 100 \text{ grams} = 0.1 \text{ kg}$, THEN

$$W = mg = (0.1 \text{ kg})(9.8 \text{ m/s}^2) = 0.98 \text{ N}$$

BUT $1 \text{ N} = 10^5 \text{ DYNES}$, SO

$$\underline{W = 98,000 \text{ DYNES}}$$

(e.) THIS IS A CONVERSION FROM MASS TO FORCE AND FROM SI TO ENGLISH UNITS. SINCE $m = 200 \text{ kg}$ AND $g = 9.8 \text{ m/s}^2$, WE HAVE

$$W(F) = mg = (200 \text{ kg})(9.8 \text{ m/s}^2) \\ = 1960 \text{ N}$$

SINCE $1 \text{ N} = 0.2248 \text{ lb}_f$ WE HAVE

$$\underline{W(F) = 440.6 \dots \text{lb}_f}$$

2.6 (a.) VOLUME = $V = \pi \times \frac{(\text{DIAMETER})^2}{4} \times \text{LENGTH}$

$$V = \pi \left(\frac{1m^2}{4} \right) (1.5m) = \underline{1.178 \dots m^3}$$

(b.) SPECIFIC WEIGHT = $\gamma = \frac{W}{V} = \frac{6000 \text{ N}}{1.178 \text{ m}^3} = 8$

$$\underline{\gamma = 5093 \text{ N/m}^3}$$

(c.) DENSITY = $\rho = m/V = W/gV = \gamma/g$

$$\rho = \frac{5093 \text{ N/m}^3}{9.82 \text{ N/kg}} = \underline{\underline{518.6 \text{ kg/m}^3}}$$

(d) SPECIFIC GRAVITY $S.G. = \rho/1000$
 $S.G. = 0.5186\dots$

2.7 $W=mg$ AND $V=mr$. THEN $m=V/v$ AND
 $W=Vg/v$. SUBSTITUTING VALUES:

$$W = \frac{(4800 \text{ cm}^3)(9.78 \text{ m/s}^2)(10^{-6} \text{ m}^3/\text{cm}^3)}{0.9 \text{ m}^3/\text{kg}}$$

$$\underline{\underline{W = 0.052\dots \text{ N}}}$$

2.8 (a.) $P = P_g + \text{atmospheric pressure}$
 $P = 1.0 \text{ kPa} + 101 \text{ kPa} = \underline{\underline{102 \text{ kPa}}}$

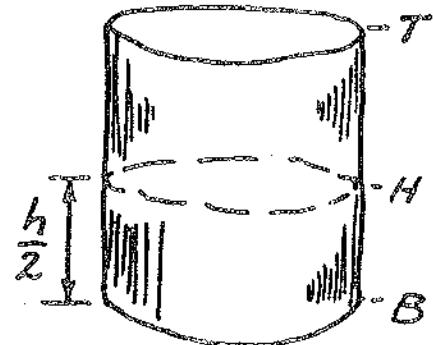
(b.) IF atmospheric pressure = 768 mm Hg
 $1 \text{ mm Hg} \approx 0.1333 \text{ kPa}$
AND THEN

$$P = 1.0 \text{ kPa} + 768 \times 0.1333 \text{ kPa}$$

$$\underline{\underline{P = 103.39 \text{ kPa} \approx 103.4 \text{ kPa}}}$$

2.9 A TANK IS 5m HIGH AND HALF-FULL OF WATER.

(a.) ASSUME AIR PRESSURE
IS CONSTANT AT 13 kPa
IN TOP HALF OF TANK.
THEN THE GAGE
PRESSURE IS THE SAME
AT THE TOP OF THE WATER.



$$P_H = \underline{13 \text{ kPa}}$$

(b.) PRESSURE AT BOTTOM = $P_B = P_H + \gamma_{H_2O} \frac{h}{2}$

$$P_B = 13 \text{ kPa} + (998 \frac{\text{kg}}{\text{m}^3} \times 9.8 \frac{\text{m}}{\text{s}^2})(2.5 \text{ m})$$

$$= 13 \text{ kPa} + 24.451 \text{ kPa} = \underline{37.451 \text{ kPa}}$$

(c.) $P_H = 13 \text{ kPa} + 101 \text{ kPa} = \underline{114 \text{ kPa}}$
 $P_B = 37.451 + 101 = \underline{138.451 \text{ kPa}}$

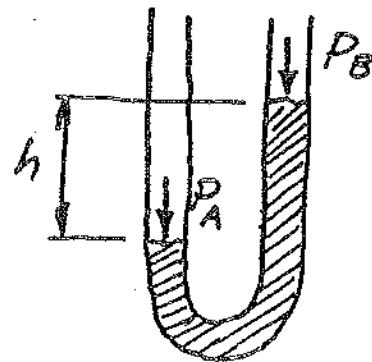
2.10 (a.) DENSITY $\rho = \frac{1}{\gamma} = \frac{1}{10.07 \text{ ft}^3/\text{lb}_m} = \underline{.0993 \text{ lb}_m/\text{ft}^3}$

(b.) SPECIFIC WEIGHT $\gamma' = \frac{g_c}{g_e} \rho$
 $\gamma' = \left(\frac{32.1 \text{ ft/s}^2}{32.174 \text{ ft.lbm/lbf.s}^2} \right) (.0993 \frac{\text{lb}_m}{\text{ft}^3})$

$$\gamma' = \underline{.0991 \text{ lb}/\text{ft}^3}$$

$$(c.) \text{SPECIFIC GRAVITY} = \rho / 62.43 = .00159$$

2.11 AIR IS ASSUMED TO HAVE A CONSTANT PRESSURE THROUGHOUT ANY ONE CLOSED VOLUME SO THAT P_A ACTS ON MERCURY IN MANOMETER AS SHOWN. THE PRESSURE IN THE MERCURY IS THE SAME AT ANY ONE ELEVATION. THUS

$$P_A = P_B + \frac{\gamma}{Hg} \times h$$


SOLVING FOR h :

$$h = \frac{P_A - P_B}{\frac{\gamma}{Hg}} = \frac{(20 \text{ psig} - 18 \text{ psig})(144 \text{ in}^2/\text{ft}^2)}{(845 \text{ lb}/\text{ft}^3)}$$

$$\underline{h = 0.34 \text{ ft}}$$

2.12 PRESSURE = FORCE/AREA

FORCE = PRESSURE \times AREA

$$= (250 \frac{\text{lb}}{\text{in}^2}) (\pi) \left(\frac{1 \text{ ft}^2}{4}\right) (144 \text{ in}^2/\text{ft}^2)$$

$$\underline{= 28,274 \text{ lb}_f}$$

$$2.13 \text{ (a.) } \underline{14.8 \text{ psiv}}$$

$$\text{(b.) } \underline{14 \text{ in. Hg vacuum}}$$

$$2.14 \text{ (a.) } \underline{14.7 \text{ psi} = 29.9389... \text{ in Hg}}$$

$$\text{(b.) } \underline{460 \text{ mm Hg} = 61.3... \text{ kPa}}$$

$$\text{(c.) } \underline{300 \text{ in. Hg} = 147.3 \text{ psi}}$$

$$\text{(d.) } \underline{50 \text{ psi} = 344.75 \text{ kPa}}$$

$$\text{(e.) } \underline{20 \text{ kPa} = 2.9008 \text{ psi}}$$

$$\text{(f.) } \underline{20 \text{ inches WG} = 0.722 \text{ psig}}$$

$$\text{(g.) } \underline{50 \text{ cm WG} = 4.903 \text{ kPa}}$$

$$\begin{aligned} 2.15 \quad P &= P_g + P_a \\ &= 955 \text{ psig} + 14.4 \text{ psi} \\ &= \underline{969.4 \text{ psia}} \end{aligned}$$

$$\begin{aligned} 2.16 \quad P &= P_a - P_{gv} = 100.4 - 80 \\ &= \underline{20.4 \text{ kPa}} \end{aligned}$$

PROBLEMS FROM SECTIONS 2.9 AND 2.10
ARE INTENDED TO HELP STUDENTS UNDER-
STAND THERMAL EQUILIBRIUM AND TEM-
PERATURE MEASUREMENTS.

2.17 BLOCKS A AND B ARE NOT IN THERMAL
EQUILIBRIUM. THEY WOULD BE IN
THERMAL EQUILIBRIUM IF THEY WERE
AT THE SAME TEMPERATURE.

2.18 COPPER-CONSTANTAN THERMOCOUPLE
WILL GENERATE AN EMF (VOLTAGE) IN
DIRECT PROPORTION TO THE JUNCTION
TEMPERATURE. THE MAXIMUM VOLT-
AGE WILL BE OBSERVABLE AT 400°F
AND FROM TABLE 2-3 THIS WOULD
BE 9.523 MILLIVOLTS.

2.19 IRON-CONSTANTAN THERMOCOUPLE HAS A
MEASURED EMF OF 8.700 mV. FROM
TABLE 2-3 THE TEMPERATURE MAY BE
FOUND BY LINEAR INTERPOLATION

$$\frac{T-177}{148.9-177} = \frac{8.700 - 9.483}{7.947 - 9.483} = .50977$$

$$\underline{T = 177 - 14.325 = 162.675^\circ C}$$

2.20 WE MAY WRITE $T_N = mT_C + b$
 WHERE m AND b ARE CONSTANTS. THEN
 WE SUBSTITUTE VALUES, $T_N = 0$ WHEN $T_C =$
 $28.5^\circ C$ AND $T_N = 100$ WHEN $T_C = 690^\circ C$.

$$0 = m(28.5) + b$$

$$100 = m(690) + b$$

SOLVING THESE TWO EQUATIONS FOR m
 AND b : $m = 0.1512$ AND $b = -4.308$
 SO THAT

$$\underline{T_N = 0.1512T_C - 4.308}$$

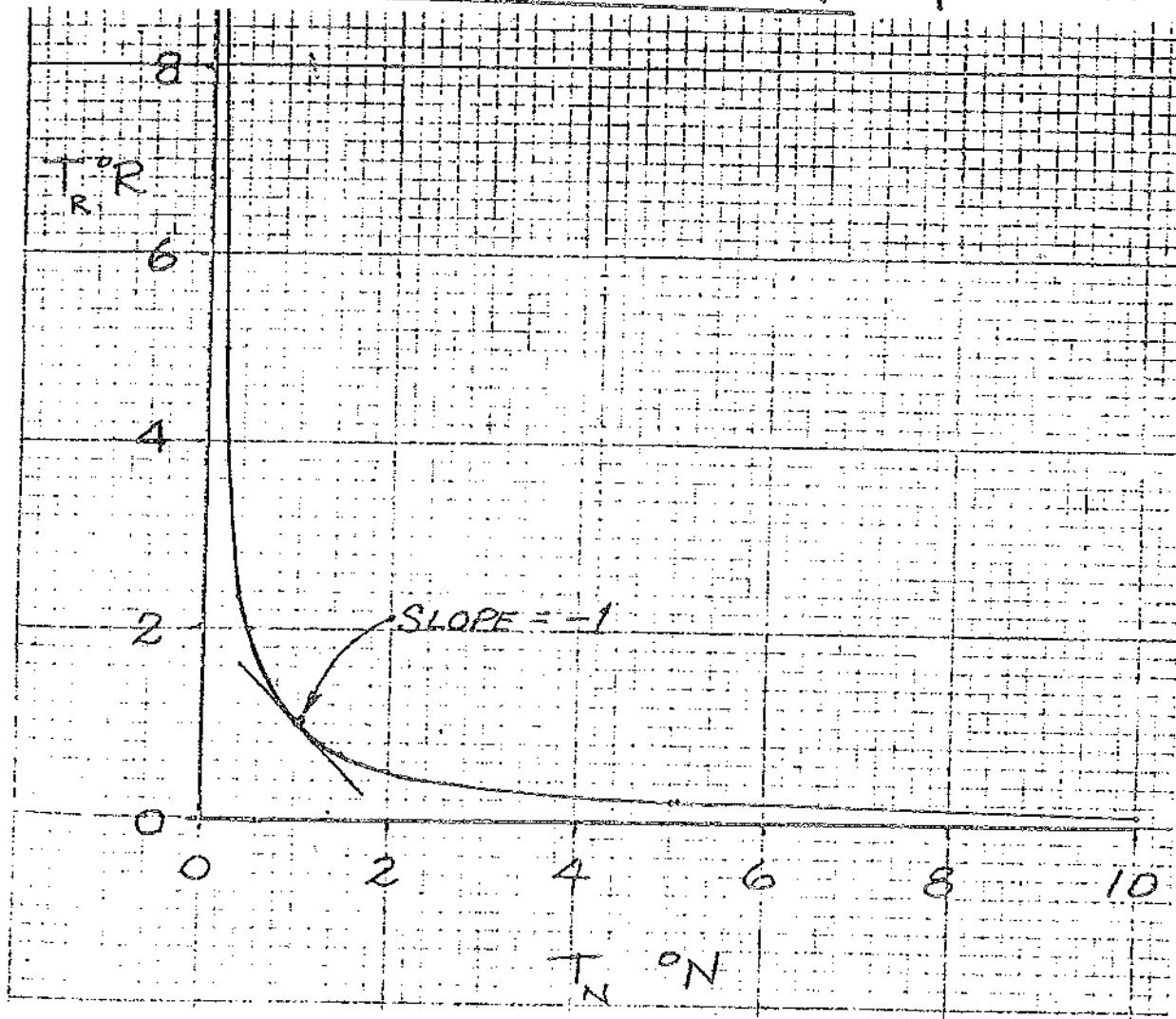
ALSO $T_C = T - 273$ WHERE T IS IN
 KELVIN DEGREES. AT ABSOLUTE ZERO;
 $T = 0$ SO

$$\underline{T_N = .1512(T - 273) - 4.308}$$

$$\underline{T_N = -45.58^\circ N}$$
 AT ABSOLUTE ZERO.

2.21 SLOPE AT $T_0 = 1^\circ D$:

$$\text{SLOPE} = -1^\circ D/R \quad (\text{SEE GRAPH})$$



2.22 $T_L = \log T^o R = \log T_K$. ALSO
 $T_K = \frac{9}{5} T_N$ SO THAT

$$T_L = \log\left(\frac{9}{5} T_K\right) = \log \frac{9}{5} + \log T_K$$

OR

$$\underline{T_L = 0.255... + \log T_K}$$

2.23 (a.) $140^{\circ}\text{F} = 600^{\circ}\text{R}$

(b.) $88^{\circ}\text{F} = 548^{\circ}\text{R}$

(c.) $230^{\circ}\text{F} = 110^{\circ}\text{C}$

(d.) $87\text{K} = 156.6^{\circ}\text{R}$

2.24 (a.) $412^{\circ}\text{F} = 872^{\circ}\text{R} = 484\text{K}$

(b.) $32^{\circ}\text{F} = 492^{\circ}\text{R} = 273\text{K}$

(c.) $117^{\circ}\text{C} = 390\text{K} = 702^{\circ}\text{R}$

(d.) $72^{\circ}\text{C} = 345\text{K} = 621^{\circ}\text{R}$

2.25 USING TABLE 2-3, THE emf IN mV FOR A COPPER-ZE-CONSTANTIN THERMOCOUPLE IS 3.967 mV AT 200°F . A THERMOPILE IS A GROUP OF THERMOCOUPLES CONNECTED IN SERIES. thus THE emf FOR 8 THERMOCOUPLES IS

$$\text{emf} = 8 \times 3.967 \text{mV}$$
$$= 31.736 \text{mV}$$

THE PROBLEMS OF SECTION 2.11 ARE INTENDED TO GIVE A BETTER UNDERSTANDING OF ENERGY : KINETIC, POTENTIAL, AND INTERNAL.

$$2.26 \text{ (a.) KINETIC ENERGY} = \frac{1}{2} m \bar{V}^2$$

$$KE = \left(\frac{1}{2} \right) (45,000 \text{ kg}) \left(1000 \frac{\text{km}}{\text{h}} \right)^2 \left(\frac{1 \text{ h}}{3600 \text{ s}} \right)^2$$

$$\text{AND } 1000 \text{ m} (10^3 \text{ m}) = 1 \text{ km SO THAT}$$

$$KE = \left(1736 \frac{\text{kg} \cdot \text{km}^2}{\text{s}^2} \right) \left(10^6 \frac{\text{m}^2}{\text{km}^2} \right) = \underline{\underline{1.736 \times 10^6 \text{ kJ}}}$$

$$(b.) \text{ POTENTIAL ENERGY} = mgz$$

$$= (45,000 \text{ kg}) (9.81 \frac{\text{m}}{\text{s}^2}) (3000 \text{ m})$$

$$PE = \underline{\underline{13.2435 \times 10^5 \text{ kJ}}}$$

2.27 (a.) ZERO (0), SINCE \bar{V} APPEARS TO BE ZERO.

$$(b.) KE = \frac{1}{2} m \bar{V}^2 = \frac{1}{2} \left(\frac{W}{g} \right) \bar{V}^2$$

$$= \left(\frac{1}{2} \right) \left(\frac{170 \text{ N}}{9.8 \text{ m/s}^2} \right) \left(140,000 \frac{\text{m}}{\text{h}} \right)^2 \left(\frac{1 \text{ h}}{3600 \text{ s}} \right)^2$$

$$KE \approx \underline{\underline{13,100 \text{ kJ}}}$$

2.28 (a.) THE WOOD WILL FALL 40 meters. THUS

$$\Delta PE = mg(\Delta z) = (1\text{kg})(9.8 \frac{\text{m}}{\text{s}^2})(40\text{m}) \\ = \underline{392 \text{ J}}$$

(b.) THE STEEL WILL SINK AND THEREFORE FALL 60 meters.

$$\Delta PE = (1\text{kg})(9.8 \frac{\text{m}}{\text{s}^2})(60\text{m}) = \underline{588 \text{ J}}$$

2.29 THE ENERGY SUPPLIED BY THE PUMP MUST BE EQUAL TO THE INCREASE IN POTENTIAL ENERGY OF THE WATER, WHICH IS

$$\Delta pe = \Delta PE/m = g(\Delta z) \\ = (9.8 \frac{\text{m}}{\text{s}^2})(75\text{m}) = \underline{735 \text{ J/kg}}$$

2.30 $ke = \frac{1}{2} \bar{V}^2 = \left(\frac{1}{2}\right)\left(24 \frac{\text{m}}{\text{s}}\right)^2 = \underline{288 \text{ J/kg}}$

2.31 $KE = \frac{1}{2} m \bar{V}^2 = \frac{1}{2}(1\text{kg})\left(60 \frac{\text{m}}{\text{s}}\right)^2 = \underline{1800 \text{ J}}$

2.32 (a.) TOTAL ENERGY = $AKE + KE + PE + U$
 $= \underline{305 \text{ kJ}}$

$$(b.) \text{ TOTAL MECHANICAL ENERGY} = \text{AKE} + \text{KE} \\ * \text{PE} \\ = \underline{\underline{270 \text{ kJ}}}$$

2.33 (a.) POTENTIAL ENERGY, $\text{PE} = mgz/g_c$

AND $g = 32.09 \text{ ft/s}^2$ FROM TABLE B.2
THE BALLOON MASS IS

$$m = \frac{g_c}{g} W = \left(\frac{32.17}{31.7} \right) \left(\frac{10}{16} \text{ lb}_f \right) = 0.634 \text{ lb}_m$$

THEN

$$\text{PE} = mgz/g_c = \frac{(0.634 \text{ lb}_m)(32.09 \text{ ft/s}^2)(5000 \text{ ft})}{(32.17 \text{ ft/lbm/lbf.s}^2)}$$

$$\underline{\underline{\text{PE} = 3162.1 \text{ ft-lbf}}}$$

(b.) AT SEA LEVEL $g = 32.108$ FROM
TABLE B.2. THEN, WITH $z = -1000 \text{ ft}$

$$\text{PE} = \frac{(0.634 \text{ lb}_m)(32.108 \text{ ft/s}^2)(-1000 \text{ ft})}{(32.17 \text{ ft/lbm/lbf.s}^2)} \\ = \underline{\underline{-632.778 \text{ ft-lbf}}}$$

(c.) zero, SINCE RELEASE POINT WAS
ASSUMED TO BE ELEVATION OF
ZERO POTENTIAL ENERGY.

$$\begin{aligned}
 2.34 \text{ TOTAL ENERGY} &= KE + PE + U \\
 &= 28 \text{ BTU} + 2 \text{ BTU} + 150 \text{ BTU} \\
 &= \underline{\underline{180 \text{ BTU}}}.
 \end{aligned}$$

$$\begin{aligned}
 2.35 \quad KE &= \frac{1}{2} \bar{V}^2 = \frac{(70 \text{ mi/hr})^2 (1.47 \text{ ft/s/mi/hr})^2}{(2)(32.17 \text{ ft-lbm/lbf.s}^2)} \\
 &\underline{\underline{KE = 164.5 \text{ ft-lbf/lbm}}}
 \end{aligned}$$

$$\begin{aligned}
 2.36 \text{ TOTAL ENERGY, } E &= KE + PE + U \\
 &= (10 \text{ lbm})(500 \text{ BTU/lbm}) + (10 \text{ lbm})(100 \text{ BTU/lbm}) \\
 &\quad + 15,000 \text{ BTU} \\
 &\underline{\underline{E = 21,000 \text{ BTU}}}
 \end{aligned}$$

$$\underline{\underline{e = \frac{E}{m} = 2,100 \text{ BTU/lbm}}}$$

$$\begin{aligned}
 2.37 \text{ DIFFERENCE IN ENERGY} &= \Delta PE = \frac{g h}{g_e} \\
 \underline{\underline{\Delta PE = 50 \text{ ft-lbf/lbm}}} &\text{ MORE AT (1) THAN AT (2)}
 \end{aligned}$$

$$\begin{aligned}
 2.38 \quad KE &= \frac{1}{2} \bar{V}^2 = \frac{(2 \text{ ft/s})^2}{2(32.17 \text{ ft-lbm/lbf.s}^2)} \\
 &= \underline{\underline{0.062 \text{ ft-lbf/lbm}}}
 \end{aligned}$$

2.39 $pe = 150 \text{ ft-lbf/lbm}$ AT (1)

$= 100 \text{ ft-lbf/lbm}$ AT (2)

PROBLEMS IN SECTION 2.12 ARE INTENDED TO GIVE A BETTER UNDERSTANDING OF EFFICIENCY.

2.40 EFFICIENCY, $\eta = \frac{\text{OUTPUT}}{\text{INPUT}} = 0.92$

THE INPUT IS $140,000 \frac{\text{BTU}}{\text{GAL}} \times 100 \text{ GAL}$
 $= 14,000,000 \text{ BTU}.$

THE EXPECTED OUTPUT IS

$$\text{OUTPUT} = (0.92)(14,000,000 \text{ BTU}) \\ = 12,880,000 \text{ BTU.}$$

2.41 $\eta = \frac{\text{OUTPUT}}{\text{INPUT}} = 0.08$ AND $\text{OUTPUT} = 2.5 \text{ kW}$

SO THAT $\text{INPUT} = \frac{2.5 \text{ kW}}{0.08} = 31.25 \text{ kW}$

ALSO

$$\text{INPUT} = (1000 \text{ W/m}^2)(\text{AREA OF PANEL})$$

AND

$$\text{AREA OF PANEL} = \frac{31.25 \text{ kW}}{1000 \text{ W/m}^2} = \underline{\underline{31.25 \text{ m}^2}}$$

$$2.42 \quad \eta = \frac{\text{OUTPUT}}{\text{INPUT}} = 0.70$$

THE INPUT IS THE POTENTIAL ENERGY OF THE WATER : $60 \text{ lb}_f \cdot \text{ft}/\text{lbm}$ AND THE RATE IS $60 \times 1,000,000 \text{ ft.lb/min}$
 $= 60,000,000 \text{ ft-lbf/min}$

$$\begin{aligned} &= 1,000,000 \text{ ft-lbf/s} = 1818.18\dots \text{ hp} \\ &= 1356.36\dots \text{ kW} \end{aligned}$$

THE OUTPUT IS THEN

$$\begin{aligned} \text{OUTPUT} &= (0.70)(1356.36 \text{ kW}) \\ &= \underline{949.45 \text{ kW}} \end{aligned}$$

$$2.43 \quad \text{EFFICIENCY}, \quad \eta = \frac{\text{OUTPUT}}{\text{INPUT}}$$

$$\text{OUTPUT} = 200 \text{ MW} = 200,000 \text{ kW}$$

$$\begin{aligned} \text{INPUT} &= 30,000 \frac{\text{kJ}}{\text{kg}} \times 1.6 \times 10^6 \frac{\text{kg}}{\text{day}} \\ &= 48 \times 10^9 \text{ kJ/day} = 2 \times 10^9 \text{ kJ/hr} \\ &= 555,555\dots \text{ kW} \end{aligned}$$

$$\text{so } \eta = \frac{200,000 \text{ kW}}{555,555 \text{ kW}} = \underline{36\% (.36)}$$

$$2.44 \quad \text{EFFICIENCY} = \frac{\text{OUTPUT}}{\text{INPUT}} = \eta$$

$$\text{OUTPUT} = 5 \text{ kW}$$

$$\text{INPUT} = 180,000 \frac{\text{BTU}}{\text{GAL}} \times 0.4 \frac{\text{GAL}}{\text{hr}}$$

$$\text{INPUT} = 72,000 \frac{\text{BTU}}{\text{hr}} = 20 \frac{\text{BTU}}{\text{s}}$$

$$= 21.1 \text{ kW}$$

SO THAT

$$\eta = \frac{5 \text{ kW}}{21.1 \text{ kW}} = \underline{23.7 \%}$$

$$2.45 \quad \text{EFFICIENCY} = \frac{\text{OUTPUT}}{\text{INPUT}} = \eta$$

$$\text{INPUT} = 3800 \text{ J}$$

$$\text{OUTPUT} = 3600 \text{ W.s} = 3600 \text{ J}$$

$$\text{So } \eta = \frac{3600 \text{ J}}{3800 \text{ J}} = \underline{94.7 \%}$$

$$2.46 \quad \text{FOR 100 WIND GENERATORS PRODUCING 250 kW EACH, TOTAL POWER} = 100 \times 250 \text{ kW}$$

$$= 25 \text{ MW}$$

FOR 38% EFFICIENCY

$$\eta = \frac{\text{OUTPUT}}{\text{WIND POWER}} = 0.38$$

AND

$$\text{WIND POWER} = \frac{25 \text{ MW}}{0.38}$$

$$= \underline{65.789 \text{ MW}}$$

PROBLEMS OF SECTION 2.13 ARE INTENDED TO PROVIDE ADDITIONAL PRACTICE IN HANDLING UNITS.

2.47 FROM THE DEFINING EQUATION FOR THE REYNOLDS NUMBER

$$\mu = \frac{\rho \bar{V} D}{R_e} \quad \text{AND } R_e \text{ IS UNLESS, } \rho \text{ IS DENSITY, } \bar{V} \text{ IS VELOCITY, AND } D \text{ IS A DIAMETER OR LENGTH. IN SI:}$$

$$\mu = \left(\frac{\text{kg}}{\text{m}^3} \right) \left(\frac{\text{m}}{\text{s}} \right) (\text{m}) = \underline{\underline{\text{kg}/\text{m}\cdot\text{s}}}$$

IN ENGLISH UNITS

$$\mu = \left(\frac{16\text{lb}}{\text{ft}^3} \right) \left(\frac{\text{ft}}{\text{s}} \right) (\text{ft}) = \underline{\underline{16\text{lb}/\text{ft}\cdot\text{s}}}$$

2.48 (a.) UNITS FOR χ ARE $\frac{\text{kJ}}{\text{kg}\cdot\text{s}}$ OR $\frac{\text{BTU}}{16\text{lb}\cdot\text{s}}$

(b.) χ UNITS ARE $\frac{\text{kJ}}{\text{kg}\cdot\text{K}}$ OR $\frac{\text{kJ}}{\text{kg}\cdot\text{C}}$ IN SI

$\frac{\text{BTU}}{16\text{lb}\cdot\text{R}}$ OR $\frac{\text{BTU}}{16\text{lb}\cdot\text{F}}$ IN ENGL.

(c.) χ UNITS ARE $\underline{\underline{\text{kJ}}}$ OR $\underline{\underline{\text{BTU}}}$.

(d.) χ UNITS ARE $\text{kJ} \cdot \text{kg/m}^6$ OR $\frac{\text{BTU} \cdot \text{lbm}}{\text{ft}^6}$

(e.) χ UNITS ARE $\frac{\text{kJ}}{\text{kg} \cdot \text{K}}$ OR $\frac{\text{BTU}}{\text{lbm} \cdot ^\circ\text{R}}$

2.49 IN SI, THE LEFT SIDE HAS UNITS OF kg/m^4 . THE RIGHT SIDE:

$$\frac{(\text{kg}/\text{m}^3)(\text{m}^2/\text{s}^2)}{(\text{m})(\text{kg} \cdot \text{m}/\text{s}^2 \cdot \text{N})} \left[\frac{\text{kg}/\text{m} \cdot \text{s}}{(\text{m})(\text{m}/\text{s})(\text{N}/\text{m}^2)} \right] = \text{kg}/\text{m}^4$$

SO THE UNITS ARE THE SAME. IN ENGLISH UNITS THE LEFT SIDE HAS UNITS OF lbm/ft^4 . THE RIGHT SIDE:

$$\frac{(\text{lbm}/\text{ft}^3)(\text{ft}^2/\text{s}^2)}{(\text{ft})(\text{lbm} \cdot \text{ft}/\text{lb}_f \cdot \text{s}^2)} \left[\frac{\text{lbm}/\text{ft} \cdot \text{s}}{(\text{ft})(\text{ft}/\text{s})(\text{lb}_f/\text{ft}^2)} \right] = \text{lbm}/\text{ft}^4$$

WHICH GIVES THE SAME UNITS AS THE LEFT SIDE.

$$\begin{aligned} 2.50 \text{ (a.) UNITS OF } C &= \left(\frac{N}{\text{m}^2} \right) \left(\frac{\text{m}^3}{\text{kg}} \right)^{1/7} = \frac{N \cdot \text{m}^{3/7}}{\text{kg}^{1/7}} \quad (\text{SI}) \\ &= \left(\frac{\text{lb}_f}{\text{ft}^2} \right) \left(\frac{\text{ft}^3}{\text{lbm}} \right)^{1/7} = \frac{\text{lb}_f \cdot \text{ft}^{3/7}}{\text{lbm}^{1/7}} \quad (\text{ENGLISH}) \end{aligned}$$

2.50 (cont.) (b.) $\left(\frac{N}{m^2}\right)\left(\frac{m^3}{kg}\right)^{1.3} = \frac{N \cdot m^{1.9}}{kg^{1.3}}$ (SI)

$$\left(\frac{lb_f}{ft^2}\right)\left(\frac{ft^3}{lb_m}\right)^{1.3} = \frac{lb_f \cdot ft^{1.9}}{lb_m^{1.3}}$$
 (ENGLISH)

(c.) $\left(\frac{N}{m^2}\right)\left(\frac{m^3}{kg}\right) / \left(\frac{m^3}{kg}\right)^{2.3} = \frac{N \cdot kg^{1.3}}{m^{5.9}}$ (SI)

$$\left(\frac{lb_f}{ft^2}\right)\left(\frac{ft^3}{lb_m}\right) / \left(\frac{ft^3}{lb_m}\right)^{2.3} = \frac{lb_f \cdot lb_m^{1.3}}{ft^{5.9}}$$
 (ENGL.)

(d.) N/m^2 (Pa) OR lb_f/ft^2

OR lb_f/in^2 (psi)

(e.) K OR °R