

3.1 Solu:

$$X_{16QAM}(t) = \delta_1 A_c \cos(\omega_c t + \Delta\theta) - \delta_2 A_c (1 + \epsilon) \sin \omega_c t$$

(a)  $\Delta\theta \neq 0, \epsilon = 0$

$$\begin{aligned} X_{16QAM}(t) &= \delta_1 A_c \cos(\omega_c t + \Delta\theta) - \delta_2 A_c \sin \omega_c t \\ &= \delta_1 A_c [\cos \omega_c t \cos \Delta\theta - \sin \omega_c t \sin \Delta\theta] - \delta_2 A_c \sin \omega_c t \\ &= \delta_1 A_c \cos \Delta\theta \cos \omega_c t - (\delta_1 A_c \sin \Delta\theta + \delta_2 A_c) \sin \omega_c t \end{aligned}$$

normalized coefficient:  $\delta_1 \cos \Delta\theta, -(\delta_1 \sin \Delta\theta + \delta_2)$

$$\beta_1 = \cos \Delta\theta, \beta_2 = -\sin \Delta\theta + 1; \quad \beta_1 = \cos \Delta\theta, \beta_2 = -\sin \Delta\theta + 2;$$

$$\beta_1 = \cos \Delta\theta, \beta_2 = -\sin \Delta\theta - 1; \quad \beta_1 = \cos \Delta\theta, \beta_2 = -\sin \Delta\theta - 2;$$

$$\beta_1 = -\cos \Delta\theta, \beta_2 = \sin \Delta\theta + 1; \quad \beta_1 = -\cos \Delta\theta, \beta_2 = \sin \Delta\theta + 2;$$

$$\beta_1 = -\cos \Delta\theta, \beta_2 = \sin \Delta\theta - 1; \quad \beta_1 = -\cos \Delta\theta, \beta_2 = \sin \Delta\theta - 2;$$

$$\beta_1 = 2\cos \Delta\theta, \beta_2 = -2\sin \Delta\theta + 1; \quad \beta_1 = 2\cos \Delta\theta, \beta_2 = -2\sin \Delta\theta + 2;$$

$$\beta_1 = 2\cos \Delta\theta, \beta_2 = -2\sin \Delta\theta - 1; \quad \beta_1 = 2\cos \Delta\theta, \beta_2 = -2\sin \Delta\theta - 2;$$

$$\beta_1 = -2\cos \Delta\theta, \beta_2 = 2\sin \Delta\theta + 1; \quad \beta_1 = -2\cos \Delta\theta, \beta_2 = 2\sin \Delta\theta + 2;$$

$$\beta_1 = -2\cos \Delta\theta, \beta_2 = 2\sin \Delta\theta - 1; \quad \beta_1 = -2\cos \Delta\theta, \beta_2 = 2\sin \Delta\theta - 2;$$

(b)  $\Delta\theta = 0, \epsilon \neq 0$

$$X_{16QAM}(t) = \delta_1 A_c \cos \omega_c t - \delta_2 A_c (1 + \epsilon) \sin \omega_c t$$

normalized coefficient:  $(\delta_1, -\delta_2(1 + \epsilon))$

Similar to (a), there are 16 different combinations

3.2 Solu:

If  $NF < 10 \text{ dB}$ .

$$NF = \frac{\text{Noise, out}}{A_0^2 \cdot P_{RS}}$$

$$\frac{\text{Noise, out}}{A_0^2} = \text{Noise, in} = NF \cdot P_{RS}$$

$$\begin{aligned} \therefore \text{Noise, in} \cdot B &= NF_{\text{dB}} + 174 \text{ dB/Hz} + 10 \log B \\ &= (10 - 174 + 53) \text{ dBm} \\ &= -111 \text{ dBm}. \end{aligned}$$

$$\text{If } NF < 10 \text{ dB} \Rightarrow \text{Noise, in} \cdot B < -111 \text{ dBm}.$$

$$IIP_3 = P_{in} + \frac{P_{in} - P_{IM, in}}{2}$$

Since the maximum tolerable noise is  $-108 \text{ dBm}$ ,  
the IM can contribute more than  $3 \text{ dB}$ .

$$\text{So } P_{IM, in} > -111 \text{ dBm}$$

$$\Rightarrow IIP_3 < -18 \text{ dBm}.$$

It demonstrates that if the RX contributes less noise,  
the receiver's linearity requirement can be loose.

3.3 solve:

For WCDMA,

Receiver sensitivity :  $-104 \text{ dBm}$ .

$B$  :  $5 \text{ MHz}$ .

Assum:  $NF = 3 \text{ dB}$

$$\begin{aligned} \text{Noise}_{in,B} &= -174 \text{ dBm} + 3 + 10 \log(3.84 \text{ MHz}) \\ &= -115 \text{ dBm}. \end{aligned}$$

For an acceptable BER,  $SNR$  of  $9 \text{ dB}$  is required.  
i.e. the total noise in the desired channel must remain below  $-113 \text{ dBm}$ .

$\Rightarrow$  The intermodulation can contribute at most  $2 \text{ dB}$

i.e.  $P_{IM, in} = -117 \text{ dBm}$ .

$$\begin{aligned} IIP_3 &= \frac{-46 \text{ dBm} - (-117 \text{ dBm})}{2} + (-46 \text{ dBm}) \\ &= -10.5 \text{ dBm}. \end{aligned}$$

3.4 Solu:

IMX2000. maximum tolerable relative noise floor.

In DCS1800 RX Band 1805 ~ 1880 MHz.

TX Power remain below -71 dBm, in 100-KHz bandwidth.  
of DCS1800.

$$-71 \text{ dBm} - 10 \lg(10 \text{ kHz}) = -121 \text{ dBm / Hz}.$$

Tx outpower : 24 dBm.

⇒ The Max Tolerable relative noise floor :

$$-145 \text{ dBc / Hz}.$$

3.5  
Solu:

This problem is the same as Problem 3.3.

→ 3.6 Solu:

$$\text{SNR} = 17 \text{ dB}$$

That means the total noise should remain below  $-81 \text{ dBm}$ .

Let me assume  $\text{NF} = 10 \text{ dB}$ .

$$B = 1 \text{ MHz.}$$

$$\begin{aligned} \text{Noise by Rx} &= -174 \text{ dBm/Hz} + 10 \lg B + \text{NF.} \\ &= -104 \text{ dBm.} \end{aligned}$$

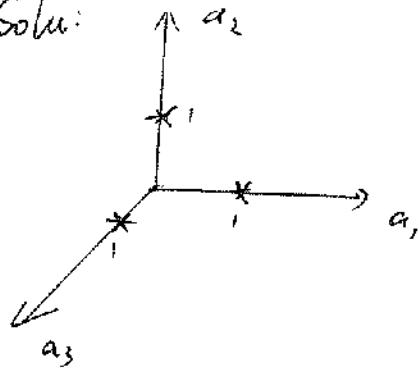
So IM can contribute maximum  $23 \text{ dB}$ .

$$\Rightarrow -81.02 \text{ dBm.}$$

$$\text{IIP}_3 = \frac{(-39) - (-81.02)}{2} \text{ dB} + (-39 \text{ dBm})$$

$$= -18 \text{ dBm.}$$

3.7 Solu:

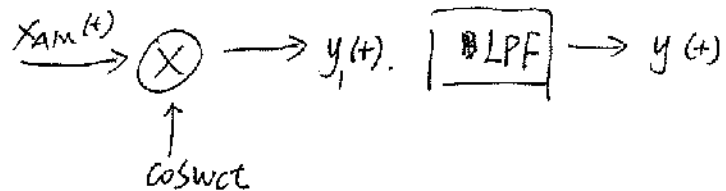


the constellation of  $X_{FSK}(t) = a_1 \cos \omega_1 t + a_2 \cos \omega_2 t + a_3 \cos \omega_3 t$ .

### 3.8 s.due:

Demodulation of AM

$$x_{AM}(t) = A_c [1 + m x_{BB}(t)] \cdot \cos \omega_c t$$



$$y_1(t) = A_c [1 + m x_{BB}(t)] \cos^2 \omega_c t$$

$$= A_c [1 + m x_{BB}(t)] \frac{1 + \cos 2\theta}{2}$$

$$y(t) = \text{LPF} [y_1(t)]$$

$$= \frac{1}{2} A_c [1 + m x_{BB}(t)]$$

From the equation of  $y(t)$ , we can easily find

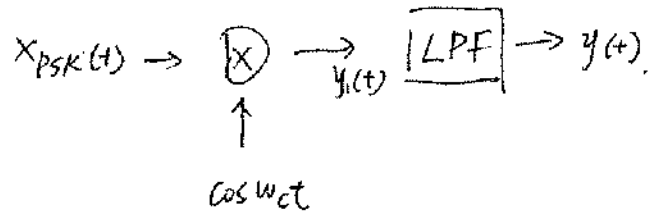
the original information  $x_{BB}(t)$ .



3.9 solve:

Demodulation of PSK

$$x_{\text{PSK}}(t) = a_n \cos \omega_c t$$



$$y_1(t) = a_n \cos \omega_c t \cdot \cos \omega_c t$$

$$= \frac{1}{2} a_n (1 + \cos 2\omega_c t)$$

$\Downarrow$

$$y(t) = \text{LPF}[y_1(t)]$$

$$= \frac{1}{2} a_n$$

From the result of  $y(t)$ , we can easily find the original binary sequence  $a_n$ .

3.60 Solu:

$$x_{\text{BPSK}}(t) = a_n \cos \omega_c t$$

Proof:

$$y_1(t) = x_{\text{BPSK}} \cdot \cos(\omega_c t + \omega_w) t.$$

$$= a_n \cos \omega_c t \cdot \cos(\omega_c t + \omega_w) t.$$

$$= \frac{1}{2} a_n [\cos(2\omega_c + \omega_w) t + \cos \omega_w t]$$

$$y(t) \stackrel{\text{LPF}}{=} [y_1(t)]$$

$$= \frac{1}{2} a_n \cos \omega_w t.$$

